



OPEN Water can trigger nuclear reaction to produce energy and isotope gases

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This paper reports the discovery that water can trigger a peculiar nuclear reaction and produce energy. Cavitation may induce unusual reactions through implosion of water vapor bubbles. Many of this research has been published formally or informally. We have conducted experiments using two reactor types made from multiple-pipe heat exchanger and found that the heat exchange process of water produces peculiar excess heat and abnormally high pressure leading to rupture of the reactor. Recently, we have tested another eight reactors. Interestingly, these reactors produce non-condensable gas. We suspected that they include ^{22}Ne and CO_2 . We used a mass spectrometer (MS) to analyze 14 gas samples collected from 8 reactors, including ten samples showing a coefficient of performance $\text{COP}_x > 1.05$ (with excess heat) and four having $\text{COP}_x < 1.05$ (without excess heat). Several methods were adopted to identify the gas content. For CO_2 identification, two methods are employed. For ^{22}Ne identification, three methods are employed. All the results confirm that isotope ^{22}Ne and regular CO_2 really exist in the output gas from reactors determined to have excess heat. We conjecture a possible mechanism to produce ^{22}Ne and CO_2 and find out that ^{12}C and isotope ^{17}O are the intermediate. They finally form isotope gases containing ^{17}O , including $\text{H}_2\text{O}-17$ (heavy-oxygen water), isotope O_2 ($^{16}\text{O}-^{17}\text{O}$), and isotope CO_2 ($^{12}\text{C}-^{16}\text{O}-^{17}\text{O}$). In the excess heat producing reactors, all these gasses were detected by MS in the absence of ^{20}Ne and ^{21}Ne . The observed isotope gases produced from reactors having excess heat verifies that water can trigger a peculiar nuclear reaction and produce energy.

Review of peculiar phenomena observed in heat exchange process of water

Possible energy production via water cavitation has been noted for a long time. It was occasionally reported formally or informally that cavitation of water may induce some form of reaction by way of implosion of water vapor bubbles which produces excess energy^{1–10}.

We have conducted experiments using two reactors made from concentric multiple-pipe heat exchanger and found that, when water is flowing through a tiny space and heated, it produces peculiar excess heat probably by cavitation and dynamic implosion of nanobubbles¹¹. Water used in the experiments is the city water filtered by reverse osmosis (RO) filter.

The first reactor (VCS)¹¹ is a triple-pipe heat exchanger (THX) (about 30 meter long) using R22 vapor from a freon compressor (3 kW input) as the heat source to heat the pressurized water (about 21 bar) flowing through a tiny channel of THX, about 2 mm gap. The water flow can be controlled as a pulse flow, about 2 to 10 cycles per minute, through a control valve. VCS was developed for 2 years with several modifications¹¹. The inlet water temperature varied between 10 and 55 °C at average flowrate around 1.2 liter/min. The compressor outlet temperature varied around 150–160 °C. Modification of VCS-1, VCS-2a, VCS-2b, VCS-2c, VCS-3 includes the change

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of pulse cycle period of water flow, the optimization of piping resistance in THX, and the change of lubrication oil of compressor which will alter the heating rate of water inside THX.

The coefficient of performance COP_x is defined as the ratio of heat output to heat input across the reactor at steady state, $(Q_{wnet} + Q_{Lx}) / (W_t - Q_L)$. The maximum COP_x obtained in VCS was 4.26, Fig. 1a. Some peculiar phenomena were observed in VCS during the tests. Abnormally high pressure (greater than 720 bar) was observed which ruptured the pressure gauges and copper pipes, Fig. 1b. Possible nuclear transmutation was found by SEM/EDX inspection of ruptured copper pipe samples (C increases 200–500%, O 300–600%, Fe 400%, and new elements P, S, Ca appears).

The second reactor (Reactor 2) is a double-pipe heat exchanger (DHX)¹¹. The pulsed water flow is heated inside the DHX by hot steam from a boiler. Shown in Fig. 2a is the performance variation during the development¹¹. The maximum COP_x obtained was 2.55. Similar pipe rupture due to extreme high pressure (greater than 240 bar) takes place when $COP_x > 2.0$. Possible nuclear transmutation in ruptured copper pipe was also observed, Fig. 2b. It was found that C increases 300%, O increases 700–800%, and Cl increases 63%.

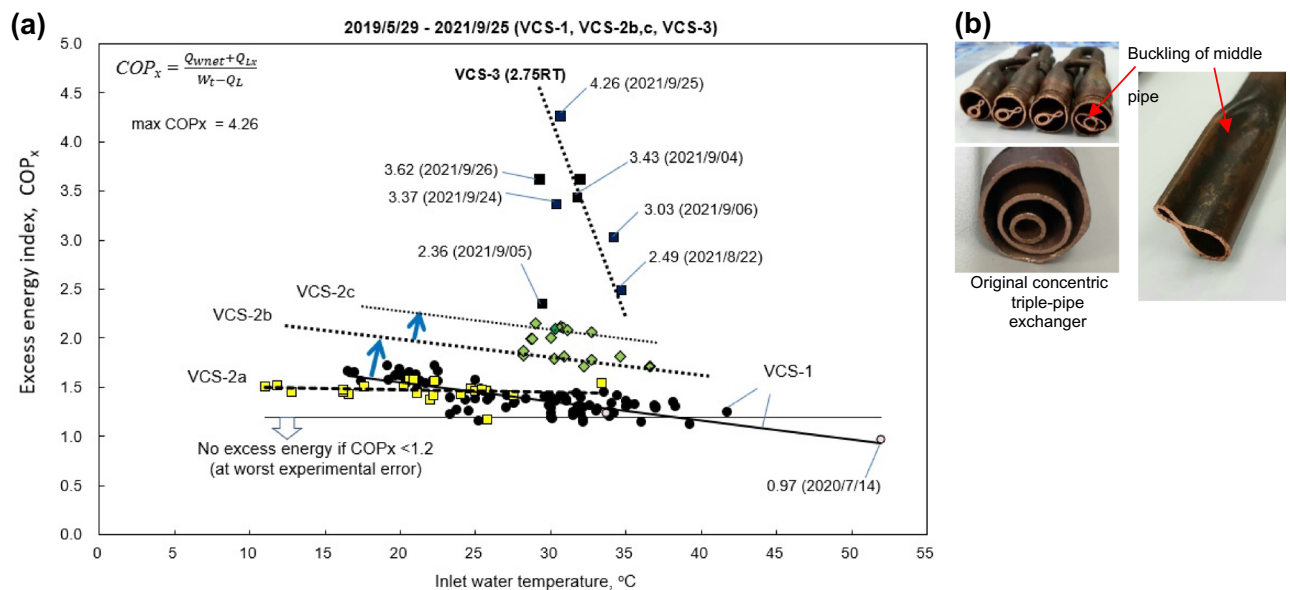


Figure 1. Test results of Reactor 1 (VCS). (a) Variation of reactor's COP_x during modifications [adding extended data of Ref.¹¹]. (b) Buckling and deformation of pipes in VCS-1 when $COP_x > 2.0$. [from Ref.¹¹].

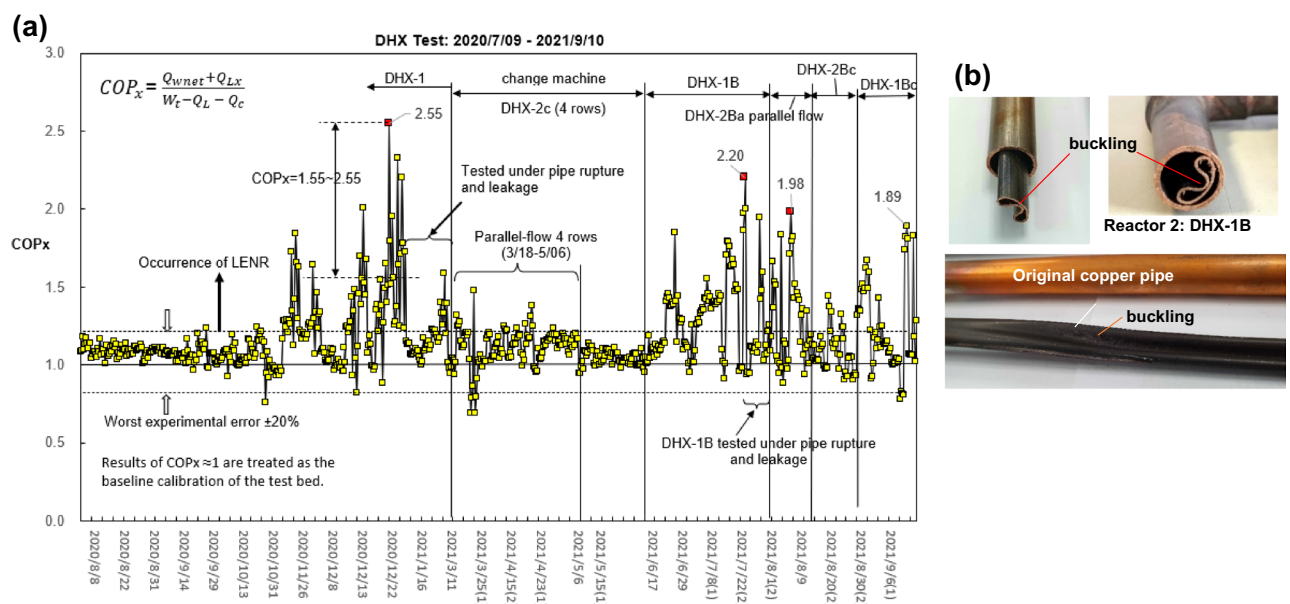


Figure 2. Test results of Reactor 2 (DHX). (a) Variation of reactor's COP_x during modifications [adding extended data of Ref.¹¹]. (b) Pipe rupture in DHX-1B when $COP_x > 2.0$ [from Ref.¹¹].

Non-condensable gases found in new reactors and analyzed

Recently, we continued to develop new reactors using thicker material and simpler structure for preventing rupture and easy scale-up. Figure 3 shows the schematic diagram of eight different new reactor designs. The new reactors are all heated by a compact once-through electric water boiler, Fig. 3h, except VCS(5RT) in which THX is heated by a hot freon vapor from compressor. The resonator-type reactors have a simple structure for easy scale-up and may create a fluid resonance to enhance the cavitation effect. The heat exchange process between two streams inside the THX or DHX does not appear in the resonator-type reactors.

The design of new reactors is briefly described as follows:

VCS(5RT): THX heated by 5 RT freon compressor and using stronger copper pipe.

VCS-NTU: THX heated by once-through water boiler and using stronger copper pipe.

DHX: same as Reactor 2 but having stronger copper pipe and with injector (nDHX).

JT1 (U-resonator): U-shape pipes with injector.

JT3 (Single-stage resonator): a single volume connected to injector.

JT4 (Jet resonator): jet impinging by two opposite injectors connected to a resonator.

JT5 (Multi-stage resonator): multiple volumes connected in series.

We also developed a new test facility, Fig. 4a, which provides a maximum power input 10 kW to the boiler and supplies boiling water at maximum temperature 190 °C to the reactors. A RO equipment with 1000L storage tank is used to supply water.

Anomalous non-condensable gases were found during the test of the reactors. We designed a gas collecting unit to collect the output gas from the reactors for analysis. A mass spectrometer manufacturer (Mastek Co,

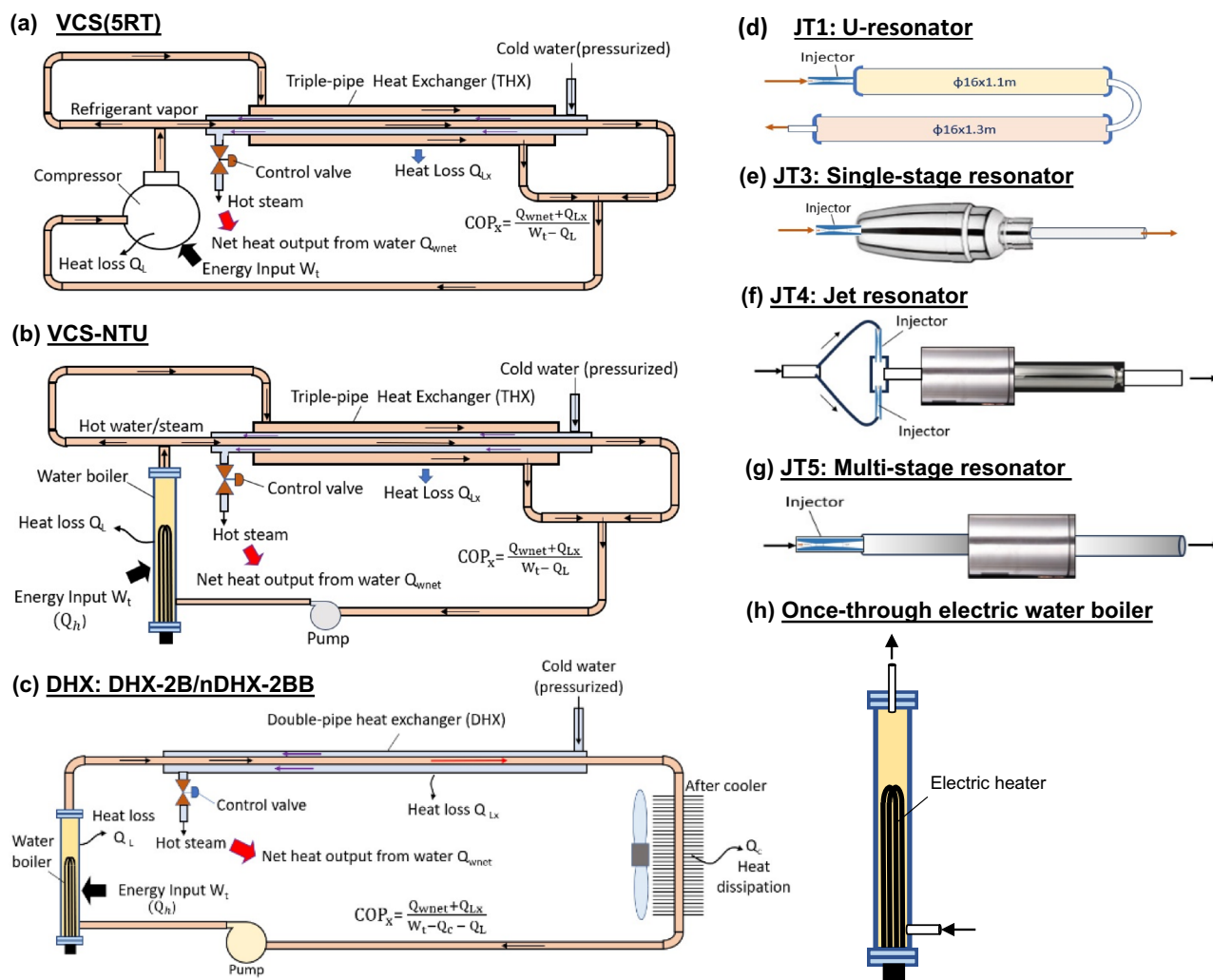


Figure 3. Reactors tested in the present study. (a) VCS(5RT): THX heated by freon from compressor; (b) VCS-NTU: THX heated by water boiler; (c) DHX: double-pipe heat exchanger heated by water boiler; (d) JT1: U-resonator; (e) JT3: single-stage resonator; (f) JT4: jet resonator; (g) JT5: multi-stage resonator; (h) once-through electric boiler to supply heat to reactors and act as a non-excess heat device. Reactors (d), (e), (f), (g) are connected to the water boiler (h) to run performance test.

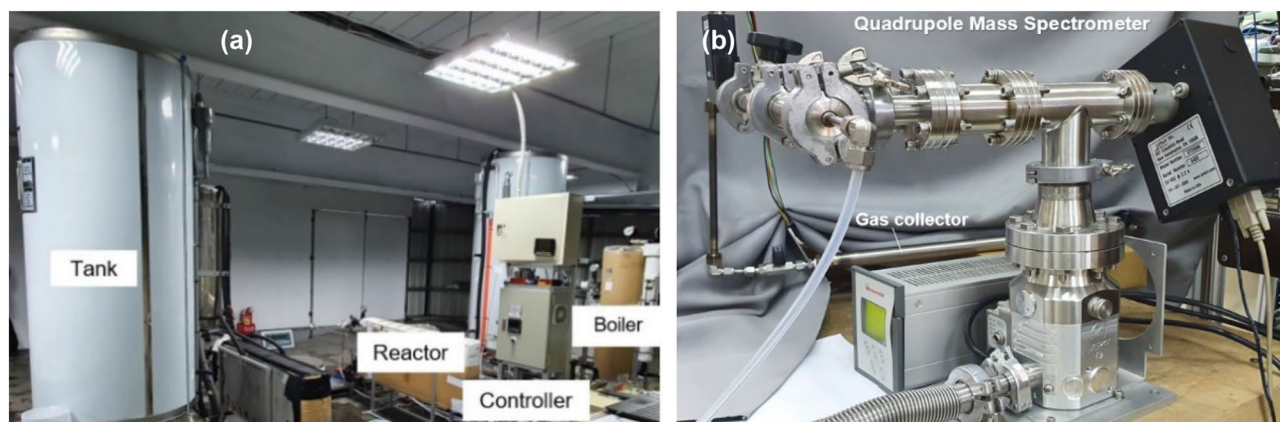


Figure 4. Test facility. (a) Performance test facility. (b) Gas collector and quadrupole mass spectrometer used.

Taiwan) and the experts team carried out the mass spectrometry. Two quadrupole mass spectrometers (model: Extorr XT200M and XT300M) were used interchangeably, as seen in Fig. 4b. The resolution of the mass spectrometer is better than 0.5 amu at 10% peak height and the minimum detectable partial pressure 5×10^{-14} Torr.

We collected gas samples from reactors running at steady state using the gas collector and then sent to manufacturer for spectrometry. The performance test was run at a steady state at least one hour to purge out the remaining impurities inside the reactor before collecting gas samples. The measuring of COP_x and thermal performance is the same as in Ref.¹¹.

Overall mass spectrum of sampled gases

At the first batch, we collected 14 gas samples (named: Tube6-Tube27) from 8 reactors for mass spectrometry. It is very interesting that the overall mass spectrum of all the gas samples have no significant m/z signals at m/z higher than 50. This means that there are no high-mass compounds in the gas samples to produce interference on lower m/z signals. And all gas samples have similar mass spectrum except the signal intensity (Fig. 5). This makes the identification of gas content using mass spectrometry much easier.

Identification of CO_2 gas

Mass spectrometer (MS) was used to analyze 14 gas samples collected from 8 reactors, 10 samples having excess heat. Four gas samples (Tube9, 12, 17, 27) are from reactors without excess heat ($COP_x < 1.05$, considering the most-probable experimental error¹¹), including Tube9 directly from the boiler (no reactor) as the reference. Tube12 and Tube27 are from failure reactor. Tube17 gas was collected during the test bed calibration using the reactor VCS-NTU under the condition of no excess heat. Table 1 lists the identification tag (ID) of gas samples and reactors of the first batch.

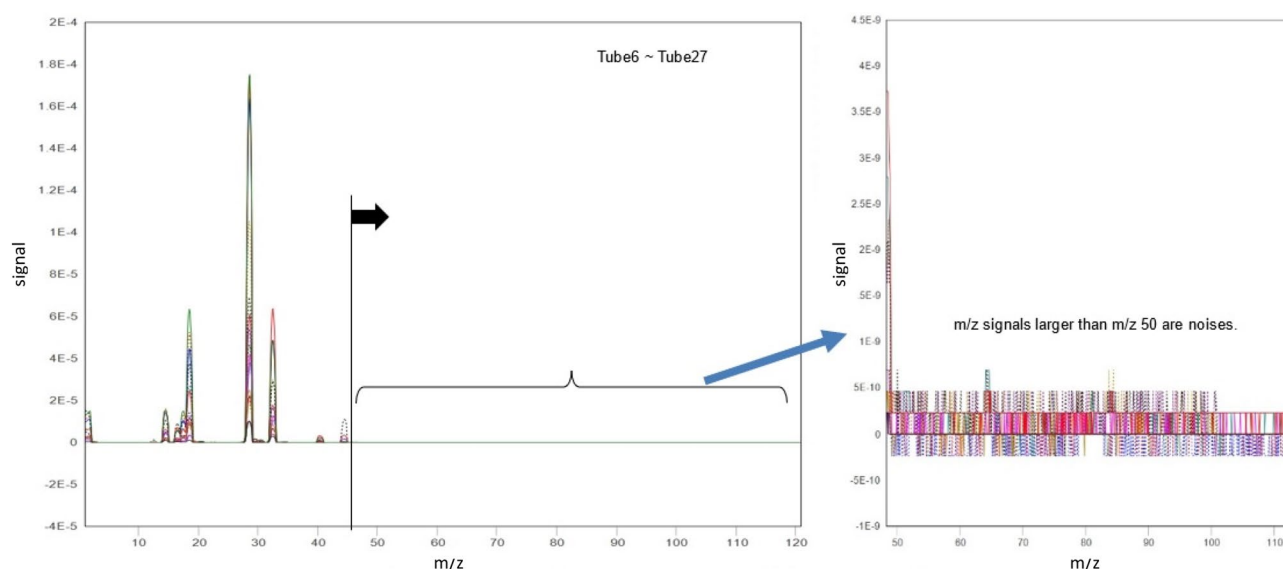


Figure 5. Overall mass spectrum of all the gas samples.

Reactor ID	Tube6	Tube7	Tube8	Tube9 (steam)	Tube10	Tube12 failure product	Tube13	Tube14	Tube 16	Tube17 baseline test	Tube 18	Tube 23	Tube 24	Tube27 failure product
Gas source (Reactor)	VCS (5RT)	VCS (5RT)	VCS (5RT)	only boiler	VCS (5RT)	JT1-n3S	DHX-2B	JT4-BV	DHX-2B	VCS-NTU(c)	JT3-CV	nDHX-2B	VCS-NTU	JT5-A5
m/z 44(gas) peak signal	4.46E-07	3.605E-06	1.89E-06	1.68E-08	7.50E-08	2.00E-08	1.50E-07	7.15E-07	1.97E-07	1.19E-07	1.90E-07	3.34E-07	1.09E-05	1.90E-07
m/z 44(air) peak signal	2.77E-07	2.857E-07	2.70E-07	1.79E-08	4.00E-08	5.10E-08	6.00E-08	5.50E-08	1.10E-07	8.01E-08	1.10E-07	1.39E-07	1.39E-07	1.39E-07
excess heat (COP _x > 1.05)	Y	Y	Y	n	Y	n	Y	Y	Y	n	Y	Y	Y	n
Measured COP _x	1.53	1.61	1.61	1.0	1.51	1.02	1.17	1.10	1.20	1.02	1.05	1.20	1.57	1.03
m/z 40(gas) peak signal	2.60E-06	3.30E-06	2.41E-06	1.24E-07	3.49E-07	1.76E-07	5.89E-07	4.96E-07	8.73E-07	6.08E-07	2.85E-07	1.34E-06	1.39E-06	1.29E-06
m/z 40(air) peak signal	2.64E-06	2.57E-06	2.57E-06	1.36E-07	4.41E-07	4.40E-07	5.21E-07	4.89E-07	9.54E-07	1.34E-07	1.37E-07	1.26E-06	1.26E-06	1.26E-06
I44(gas) = m/z 44(gas) ÷ m/z 40(gas)	0.17	1.09	0.78	0.14	0.22	0.11	0.25	1.44	0.23	0.19	0.67	0.25	7.85	0.15
I44(air) = m/z 44(air) ÷ m/z 40(air)	0.10	0.11	0.10	0.13	0.09	0.12	0.12	0.11	0.12	0.13	0.12	0.11	0.11	0.11
Internal standard ratio: K44 = I44(gas)/I44(air)	1.63	9.84	7.47	1.03	2.37	0.98	2.21	12.8	1.96	1.46	5.56	2.26	71.0	1.33
K44 > 1.5 (presence of CO ₂)	Y	Y	Y	n	Y	n	Y	Y	Y	n	Y	Y	Y	n

Table 1. Identification of CO₂ presence using isotope ratio K44. Significant values are in bold.

Two methods were employed to identify the presence of CO₂ in gas samples. First, using the isotope ratio K44 defined with respect to the background air and internal standard based on m/z 40, we can identify the presence of CO₂. The definition of K44 is $K44 = I44(\text{gas})/I44(\text{air})$, where $I44(\text{gas}) = m/z\ 44(\text{gas}) \div m/z\ 40(\text{gas})$; and $I44(\text{air}) = m/z\ 44(\text{air}) \div m/z\ 40(\text{air})$.

It is very interesting to note from Table 1 that K44 are all lower than 1.50 for gas samples from reactors without excess heat ($\text{COP}_x < 1.05$). The high isotope ratio K44 (maximum 71.0 or > 5 mostly) in gases from reactors having excess heat strongly suggests the significant presence of CO₂.

Another method to identify the CO₂ existence in gas samples is to measure m/z 44 signal reduction of gas samples which has passed through a CO₂ absorber Ca(OH)₂ before entering the mass spectrometer. Pure CO₂ gas, ambient air and MS blank were used as the reference. The rate of m/z 44 signal reduction, Ab44, for gas with (denoted as “Y”) and without (denoted as “n”) CO₂ absorption is defined as: $\text{Ab44} = m/z\ 44(\text{Y}) \div m/z\ 44(\text{n})$, and the reduction of CO₂ (r_d) is $(1 - \text{Ab44})100\%$.

Each Ab44 is measured using the identical gas sample in a gas collector. It is seen from Table 2 that Ab44 of all the gases from reactors having excess heat is lower than 1.0 or m/z 44 signal reduction is between 36 and 80%. This is the direct proof of CO₂ presence in gases from reactors having excess heat.

Identification of Neon gas ²¹Ne and ²⁰Ne

Bob Greenyer suggested that Ne (²⁰Ne, ²¹Ne, or ²²Ne) may be produced if excess heat takes place¹². First, we checked the possibility of ²¹Ne presence from the m/z 21 signal. It is seen from the mass spectrum of all gas samples shown in Fig. 6 that, no m/z 21 signal is present and hence ²¹Ne does not exist.

Since m/z 20 signal can be generated from natural abundance of Argon gas (m/z 40), the relative isotope ratio K20 (based on internal standard using m/z 40) is used to identify the presence of ²⁰Ne by comparing with the background air. The definition of isotope ratio K20 is $K20(\text{gas}) = I20(\text{gas})/I20(\text{Ar})$ where $I20(\text{gas}) = m/z\ 20(\text{gas}) \div m/z\ 40(\text{gas})$; $I20(\text{Ar}) = m/z\ 20(\text{Ar}) \div m/z\ 40(\text{Ar})$.

Pure Argon gas is used as the calibration gas whose $K20(\text{air}) = 0.76$. If $K20(\text{gas}) < K20(\text{air}) = 0.76$, it reveals that no ²⁰Ne exists in gas sample. It is seen from Fig. 7 that K20 for all gas samples are smaller than 0.76. This confirms that no ²⁰Ne is present in all gas samples, regardless of excess heat occurrence.

Identification of Neon gas ²²Ne

The presence of ²²Ne in gases from reactors having excess heat were verified using three methods:

- (1) From isotope ratio K22 based on internal standard m/z 40.
- (2) From mathematics based on the observation of parameter G > 1 in gases from reactors having excess heat.
- (3) From isotope-ratio K24a and using CO₂ absorber.

Gas sample	Reactor	COPx	CO ₂ absorption by Ca(OH) ₂	m/z 44	Ab44 = m/z 44(Y) ÷ m/z 44(n)	Reduction of m/z 44, r _d = (1 - Ab44)
Pure CO ₂	Reference gas	1.0 (No excess heat)	n	4.62E-04	0.019 (< 1)	92%
			Y	8.93E-06		
Atmosphere air	Reference gas	1.0 (No excess heat)	n	1.87E-06	1.14	n
			Y	2.14E-06		
MS blank	Reference gas	1.0 (No excess heat)	n	8.09E-06	0.98 (≈ 1.0)	n
			Y	7.96E-06		
Tube16	DHX-2B	1.20	n	1.99E-07	0.37 (< 1)	63%
			Y	7.47E-08		
Tube39	VCS-NTU	1.54	n	4.42E-06	0.74 (< 1)	36%
			Y	3.28E-06		
Tube40	VCS-NTU	1.21	n	6.70E-06	0.52 (< 1)	48%
			Y	3.51E-06		
Tube42	nDHX-2BB	1.22	n	1.68E-05	0.20 (< 1)	80%
			Y	3.40E-06		
Tube44	nDHX-2BB	1.16	n	9.98E-06	0.46 (< 1)	54%
			Y	4.62E-06		
Tube46	nDHX-2BB	1.15	n	5.52E-06	0.58 (< 1)	42%
			Y	3.20E-06		

Table 2. Identification of CO₂ presence from the reduction of m/z 44 signal caused by CO₂ absorption.

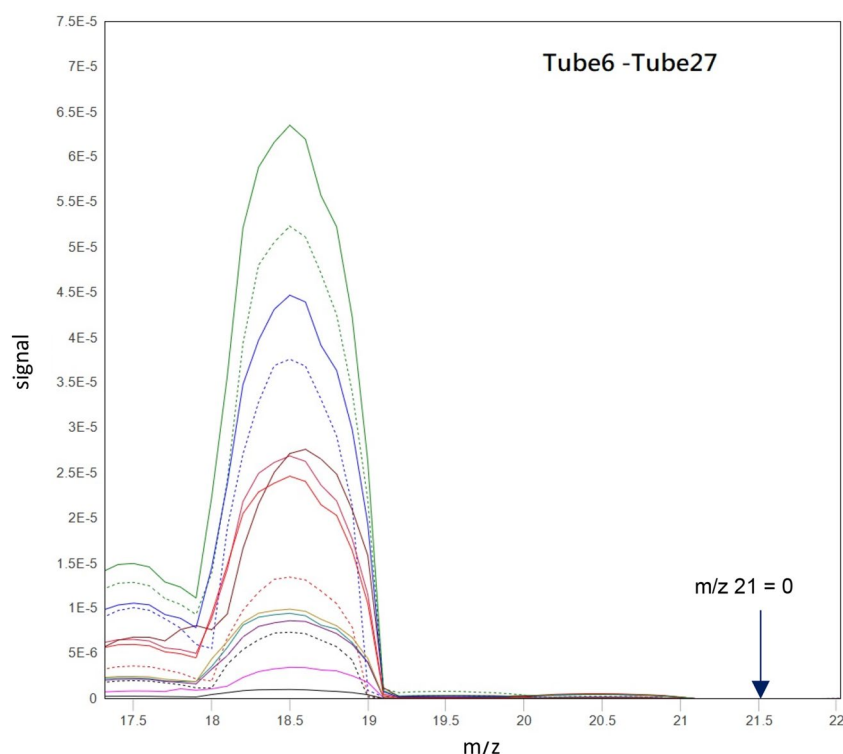


Figure 6. Mass spectrum of gas samples from m/z 17 to m/z 22 showing no m/z 21 signal at all.

Proof of ²²Ne presence from isotope ratio K22 based on internal standard m/z 40

The m/z 22 signal is generated from ²²Ne gas and CO₂⁺⁺ made by CO₂ ionization in MS, while CO₂ is the product of reactors having excess heat as described previously. The isotope ratio K22 is defined based on the internal standard m/z 40 as: $K22 = I22(\text{gas})/I22(\text{air})$, where $I22(\text{gas}) = m/z\ 22(\text{gas}) \div m/z\ 40(\text{gas})$ and $I22(\text{air}) = m/z\ 22(\text{air}) \div m/z\ 40(\text{air})$.

Since the interference of CO₂⁺⁺ on m/z 22 signal is not very high, less than 2% of m/z 44 signal for pure CO₂¹³, the isotope ratio $K22 > 1.5$ is beyond CO₂⁺⁺ interference in all gases from reactors having excess heat. The

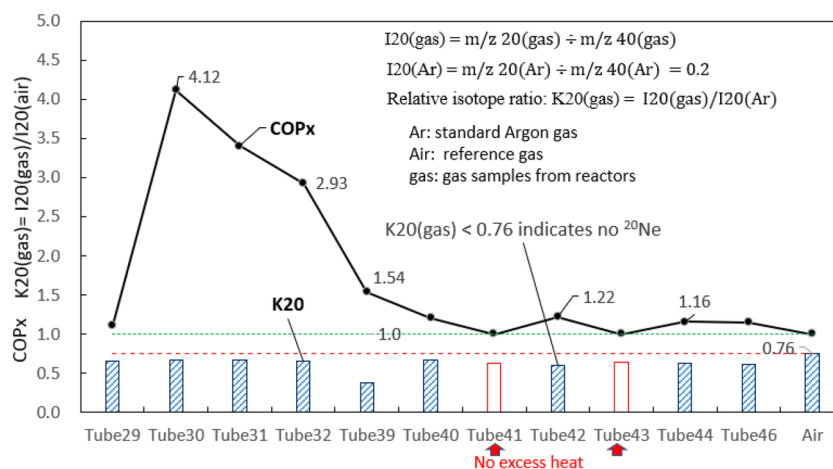


Figure 7. Variation of K20 for gas from different reactors. $K20 < 0.76$ indicates no ^{20}Ne presence.

results shown in Fig. 8 suggests that $m/z\ 22$ signal contains those generated from ^{22}Ne . Very high K22 (mostly higher than 2.0, highest 56.0) confirms that ^{22}Ne is present in gases from reactors having excess heat.

Proof of ^{22}Ne presence from mathematics based on the observation of $G > 1$ in gases having excess heat

We found an interesting parameter G defined as $G = R42(\text{gas})/R42(\text{air})$ where $R42 = m/z\ 44 \div m/z\ 22$, which is always greater than 1.0 in gases from reactors having excess heat ($\text{COP}_x > 1.05$). G can be determined from the measurement of $m/z\ 22$ and $m/z\ 44$ of gas and background air using the definition.

Since the $m/z\ 22$ signal is generated from ^{22}Ne and CO_2^{++} (ionization of CO_2 in MS), the measured $m/z\ 22$ signal is the sum of those from ^{22}Ne and those from CO_2^{++} for gas sample and background air, which can be written as

$$\begin{aligned} \text{Gas : } M_{22} &= f_i M_{44} + M_{22a} \\ \text{Air : } M'_{22} &= f_i M'_{44} + M_{22a}, \end{aligned} \quad (1)$$

where M_{22} : measured $m/z\ 22$ signal of gas, M_{22a} : $m/z\ 22$ signal contributed from ^{22}Ne , M_{44} : measured $m/z\ 44$ signal of gas, f_i : ionization factor of MS, M'_{22} : measured $m/z\ 22$ signal of background air, M'_{22a} : $m/z\ 22$ signal of background air contributed from ^{22}Ne , M'_{44} : measured $m/z\ 44$ signal of background air. We can define the excess $m/z\ 22$ signal made by ^{22}Ne in gas sample as, referring to Fig. 9a,

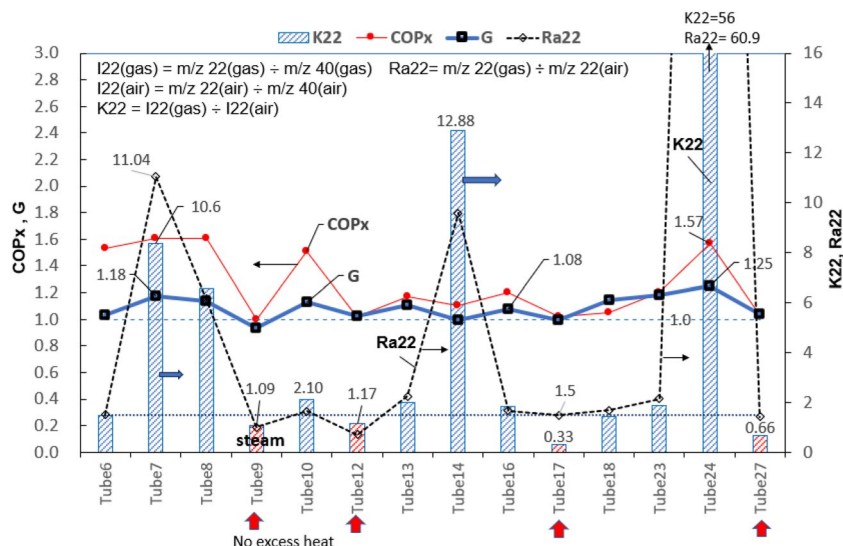


Figure 8. Variation of K22 for gas from different reactors. $K22 > 1.5$ indicates ^{22}Ne presence.

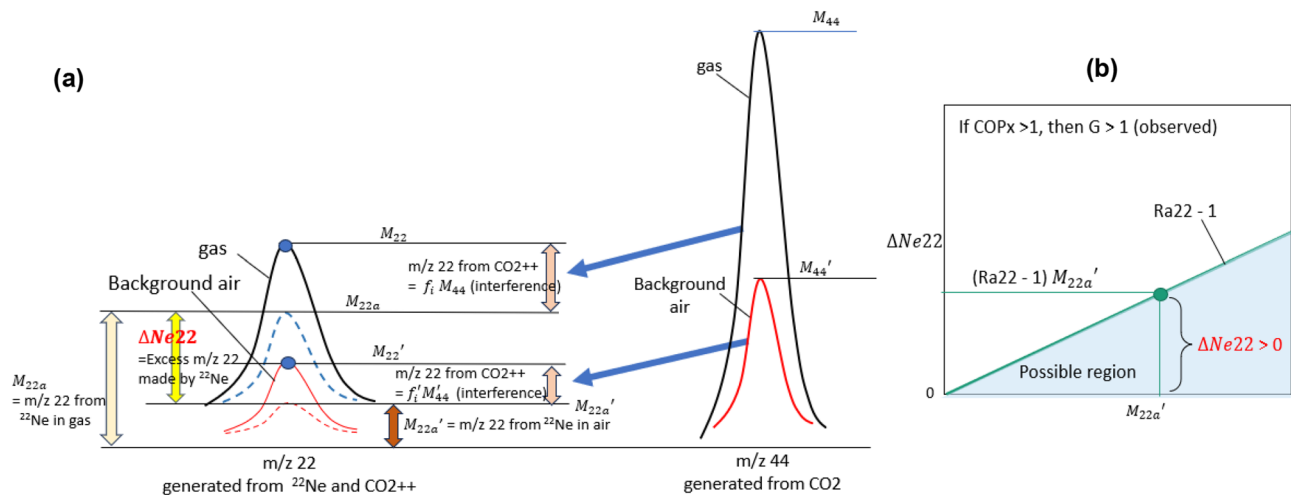


Figure 9. Graphical expression of $\Delta\text{Ne}22$. (a) Relation between m/z 22 and m/z 44. (b) The real $\Delta\text{Ne}22$ is between 0 and $(\text{Ra}22 - 1) M_{22a}'$ for $\text{Ra}22 > 1$.

$$\Delta\text{Ne}22 = M_{22a} - M_{22a}' = \text{excess m/z 22 signal generated by excess } ^{22}\text{Ne} \quad (2)$$

Combining Eqs. (1) and (2), and the observation of $G > 1$ in gases from reactors having excess heat, we obtain the following relation:

$$G = \frac{M_{22} - M_{22a}}{M_{22} - M_{22a}' \text{Ra}22} > 1 \quad (3)$$

where $\text{Ra}22 = \text{m/z 22 (gas)} \div \text{m/z 22 (air)}$. From Eq. (3), we obtain $M_{22a} < M_{22a}' \text{Ra}22$ and the following relations:

$$\Delta\text{Ne}22 = M_{22a} - M_{22a}'; \quad \frac{\Delta\text{Ne}22}{M_{22a}'} = \frac{M_{22a}}{M_{22a}'} - 1 < \text{Ra}22 - 1 \quad (4)$$

We finally obtain a relation for excess m/z 22 signal made by excess ^{22}Ne in gas sample:

$$\Delta\text{Ne}22 < (\text{Ra}22 - 1) M_{22a}' \quad (5)$$

Since $\text{Ra}22$ is experimentally found to lie between 1.5 and 60.9 for gases from reactors having excess heat as shown in Fig. 8, $(\text{Ra}22 - 1) > 0$ always and $\Delta\text{Ne}22$ is shown greater than zero. This proves the presence of ^{22}Ne in gases from reactors having excess heat. The real $\Delta\text{Ne}22$ lies between 0 and $(\text{Ra}22 - 1) M_{22a}'$ as shown in Fig. 9b.

Proof of ^{22}Ne presence from isotope-ratio K24a and using CO_2 absorber

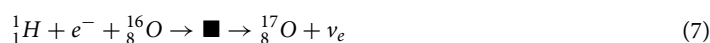
If CO_2 in gas sample is absorbed first by $\text{Ca}(\text{OH})_2$ before entering MS, m/z 22 signal interference from CO_2 can be eliminated. ^{22}Ne can be identified using the isotope ratio K24a defined as the ratio of R24 with (denoted as "Y") and without (denoted as "n") CO_2 absorption: $\text{K}24a = \text{R}24(\text{Y})/\text{R}24(\text{n})$ where $\text{R}24(\text{gas}) = \text{m/z 22}(\text{gas}) \div \text{m/z 44}(\text{gas})$.

For pure CO_2 gas, the measured $\text{K}24a(\text{CO}_2) = 0.96$. We can then identify the presence of ^{22}Ne simply from $\text{K}24a > 0.96$. It is seen from Table 3 that $\text{K}24a$ are greater than 0.96 (maximum 1.49) in all the gases from reactors having excess heat. This confirms the presence of ^{22}Ne in gases from reactors having excess heat.

We can also use another isotope ratio K22a defined as the ratio of I22 with (Y) to without (n) CO_2 absorption: $\text{K}22a = \text{I}22(\text{Y})/\text{I}22(\text{n})$ where $\text{I}22 = \text{m/z 22}(\text{gas}) \div \text{m/z 40}(\text{gas})$. The results in Table 3 shows that $\text{K}22a$ in all gases is much larger than the pure CO_2 reference (0.0060). This confirms the presence of ^{22}Ne .

Discussions

In the present study, we have verified using mass spectrometry that ^{22}Ne and CO_2 are produced in water when $\text{COP}_x > 1.05$ (having excess heat). The question remaining is how ^{22}Ne and CO_2 is produced. Since this is an unsettled area of science, we can only conjecture some possibilities based on the observed phenomena in various reactors. To find the pathway to ^{22}Ne gas production, various possible nuclear reactions could be assumed. In our judgement however, the reaction starts with an interaction between ^1H and ^{16}O , producing ^{17}O ^{14,15}. Two possible reactions for ^{17}O are proposed as follows:



									Internal standard method (ISM) based on m/z 40		
Gas sample	Reactor	COPx	CO2 absorption	m/z 22	m/z 40	m/z 44	R24= m/z 22 ÷ m/z 44	K24a= R24(Y)/ R24(n)	I22= ratio 22/40	I44= ratio 44/40	K22a= I22(Y)/ I22(n)
Pure CO ₂	Reference gas	1.0 (no excess heat)	n	4.44E-06	4.20E-07	4.62E-04	9.61E-03	0.96	10.6	1100.0	0.0060
			Y	8.26E-08	1.31E-06	8.93E-06	9.25E-03		0.0631	6.817	
Tube16	DHX-2B	1.20	n	2.33E-09	8.73E-07	1.99E-07	1.17E-02	1.07	0.0027	0.228	0.55
			Y	9.33E-10	6.37E-07	7.47E-08	1.25E-02		0.0015	0.117	
Tube39	VCS-NTU	1.54	n	2.94E-08	1.63E-05	4.42E-06	6.65E-03	1.49	0.0018	0.271	1.86
			Y	4.93E-08	9.35E-06	4.97E-06	9.92E-03		0.0053	0.532	
Tube42	nDHX-2BB	1.22	n	1.55E-07	9.78E-06	1.68E-05	9.21E-03	1.03	0.0158	1.717	0.21
			Y	3.23E-08	9.92E-06	3.40E-06	9.49E-03		0.0033	0.343	
Tube44	nDHX-2BB	1.16	n	7.75E-08	1.19E-05	9.98E-06	7.77E-03	1.14	0.0065	0.839	0.48
			Y	4.10E-08	1.30E-05	4.62E-06	8.87E-03		0.0032	0.355	
Tube46	nDHX-2BB	1.15	n	4.87E-08	1.02E-05	5.52E-06	8.82E-03	1.10	0.0048	0.541	0.65
			Y	3.10E-08	9.93E-06	3.20E-06	9.69E-03		0.0031	0.322	
							K24a > 0.96 reveals ²² Ne presence		K22a >> 0.006 reveals ²² Ne presence		

Table 3. Using isotope ratios K24a and K22a to identify the presence of ²²Ne. Significant values are in bold.

where ${}_1^1H$ represents a proton (p), $\bar{\nu}_e$ is the ultra-low energy anti-neutrino which can be produced from water cavitation¹⁶. The ‘black box’ in Eqs. (6) and (7) represents an unknown in detail mechanism¹⁵. The reaction of ${}_8^{17}O$ and ${}_8^{17}O$ then produces ²²Ne and ¹²C^{14,15}:



This is what we have detected, ²²Ne in gases from reactors having excess heat. Since ¹²C cannot exist in monoatomic form, it is converted into CO₂ through chemical reaction with ¹⁶O atoms from water, as follows:



This is what we have detected, CO₂ in gases from reactors having excess heat. The difference between Eqs. (6) and (7) is the involvement of neutrino ν_e and anti-neutrino $\bar{\nu}_e$. In Eq. (6), $\bar{\nu}_e$ acts over a wide area to allow the 4-particle reaction with ${}_1^1H, e^-, {}_8^{16}O$. That is, the low-energy anti-neutrino is the cause of increased probability of the 4-particle reaction. In Eq. (7), ν_e is the product of the 3-particle reaction which may have high energy. Since Eq. (7) involves only three-particles merging, it might be more likely to take place from the point of view of the particle collision probability if there is some way to force these particles into a confined zone. The reaction Eq. (6) is exothermic and emits no radiation. A Geiger–Müller counter (JD-3001) monitoring radiation near the reactors during test, never showed a significant emission level above background, measured at 0.4 μSv/h maximum which is about two times of background or 0.4% occurrence. This seems favor the reaction Eq. (6). In Ref.¹⁵, it is proposed from nuclear physics that neutrinos and anti-neutrino pair at low energies can be formed during inelastic collisions of particles (electrons, ions, neutral atoms) during their thermal motion. Temperatures known to be produced in cavitation processes may exceed the calculated threshold in Ref.¹⁵ for low energy neutrino and anti-neutrino pair production. The question then arises as to how the 4 particles (${}_1^1H + e^- + \bar{\nu}_e + {}_8^{16}O$) in Eq. (6) can merge simultaneously. However due to the large de Broglie wavelength of low energy neutrinos, they could probably interact over an area big enough to include all the particles necessary for reaction Eq. (6) to take place. Since the mechanism of nuclear reactions is not the focus of our research, we can only put forward intuitive and vague speculations with respect to our experimental observations. The present conjecture, reaction (6) or (7), is just two possibilities. Another question raised is that “are there extra ¹⁷O and ¹²C to produce other compounds?” Both ¹⁷O and ¹²C does not exist in monoatomic form. They will form compounds with other elements. This means that ¹²C and isotope ¹⁷O may be the intermediate. Nuclear transmutation in ruptured copper pipe with large increases of C and O contents is one of the possible outcomes and has been observed in SEM/EDS¹¹. Besides this, we found that three isotopes may be the outcomes: H₂O-17 (heavy-oxygen water), isotope O₂ (¹⁶O–¹⁷O), and isotope CO₂ (¹²C–¹⁶O–¹⁷O). This can be identified from isotope ratio analyses in m/z 19, 33 and 45 signals.

Finding of H₂O-17 (heavy-oxygen water)

The isotope ratio R198 using internal standard m/z 40 is defined as $R198 = L198(\text{gas})/L198(\text{air})$ where $L198(\text{gas}) = I19(\text{gas})/I18(\text{gas})$, $L198(\text{air}) = I19(\text{air})/I18(\text{air})$, and $I18(\text{gas}) = m/z\ 18(\text{gas}) \div m/z\ 40(\text{gas})$, $I18(\text{air}) = m/z\ 18(\text{air}) \div m/z\ 40(\text{air})$; $I19(\text{gas}) = m/z\ 19(\text{gas}) \div m/z\ 40(\text{gas})$, $I19(\text{air}) = m/z\ 19(\text{air}) \div m/z\ 40(\text{air})$.

The m/z 19 signal may be generated from HDO (deuterium water) and isotope H₂O-17. Since steam (Tube9) has highest content of HDO (deuterium water), the measured R198(steam) = 1.10 is the maximum contribution of HDO to m/z 19. This is used to distinguish H₂O-17 from HDO.

LL198 is further defined as $LL198 = R198/R198(\text{steam})$ to provide a criterion to identify the presence of H₂O-17 when $LL198 > 1.0$. It is seen from Fig. 10 that $LL198 \gg 1$ appearing in 9 out of 10 gases from reactors having excess heat. This strongly suggests significant contribution to m/z 19 from H₂O-17, other than HDO. The presence of heavy-oxygen water H₂O-17 is thus confirmed.

Tube12 gas contains no ²²Ne and CO₂ (implying no excess heat), but produces isotope H₂O-17 as seen from Fig. 10. Tube12 gas was collected from U-resonator (JT1) without excess heat ($COP_x < 1.05$). However, we found that the reactor showed abnormal temperature variations. It involves some other peculiar phenomena and needs further studies.

Finding of isotope O₂ (¹⁶O-¹⁷O)

To trace isotope O₂ (¹⁶O-¹⁷O), we define the isotope ratio K33 using internal standard m/z 40 as: $K33 = I33(\text{gas})/I33(\text{air})$ where $I33(\text{gas}) = m/z\ 33(\text{gas}) \div m/z\ 40(\text{gas})$; $I33(\text{air}) = m/z\ 33(\text{air}) \div m/z\ 40(\text{air})$. It is seen from Fig. 11, $K33 > 1.1$ in all gases from reactors having excess heat. This strongly suggests the presence of isotope O₂ (¹⁶O-¹⁷O). Again, Tube12 contains no ²²Ne and CO₂ gas but isotope O₂ (¹⁶O-¹⁷O) is present as seen from Fig. 11. This implies that some other peculiar phenomena may take place in U-resonator (JT1) and is worth for further investigations.

Finding of isotope O₂ (¹⁶O-¹⁷O)

To trace isotope CO₂ (¹²C-¹⁶O-¹⁷O), we define the isotope ratio K45 using internal standard m/z 40: $K45 = I45(\text{gas})/I45(\text{air})$ where $I45(\text{gas}) = m/z\ 45(\text{gas}) \div m/z\ 40(\text{gas})$; $I45(\text{air}) = m/z\ 45(\text{air}) \div m/z\ 40(\text{air})$. It is seen from Fig. 12, $K45 > 1.5$ takes place in gases from reactors having excess heat. High value of K45 (2.1–75) strongly suggests the presence of isotope CO₂ (¹²C-¹⁶O-¹⁷O).

Conditions for presence of isotopes H₂O-17 (heavy-oxygen water), CO₂(¹²C-¹⁶O-¹⁷O), O₂(¹⁶O-¹⁷O)

The presence of isotopes O₂ and CO₂ relies on the extra quantities of ¹²C and ¹⁷O resulting from the main nuclear reactions. Sometimes they may not appear due to no extra ¹²C or ¹⁷O. Tube7 in Fig. 6 may be the case. Nevertheless, the above results cannot deny the possible presence of isotopes O₂, CO₂ and H₂O-17 (heavy-oxygen water) in gases from reactors having excess heat.

Finally, it should be noted that the reactors tested in the present study were under early developing stage. Although their performance has not been optimized yet, the anomalous gas produced from reactors having excess heat is always present. The reactor is still being optimized to improve the performance. A higher concentration of non-condensable gases may be expected. This will make the MS analysis easier.

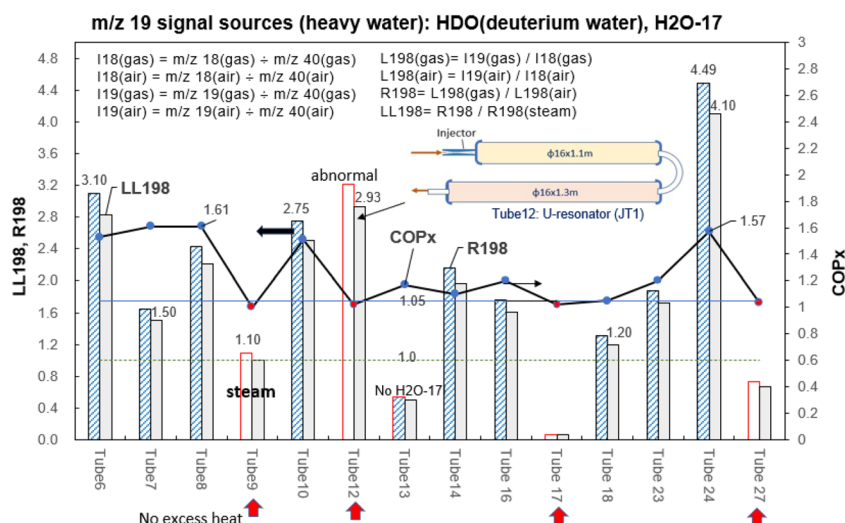


Figure 10. Variation of R198 and LL198 for gas from different reactors. Using isotope ratios R198 and LL198 to distinguish H₂O-17 from HDO.

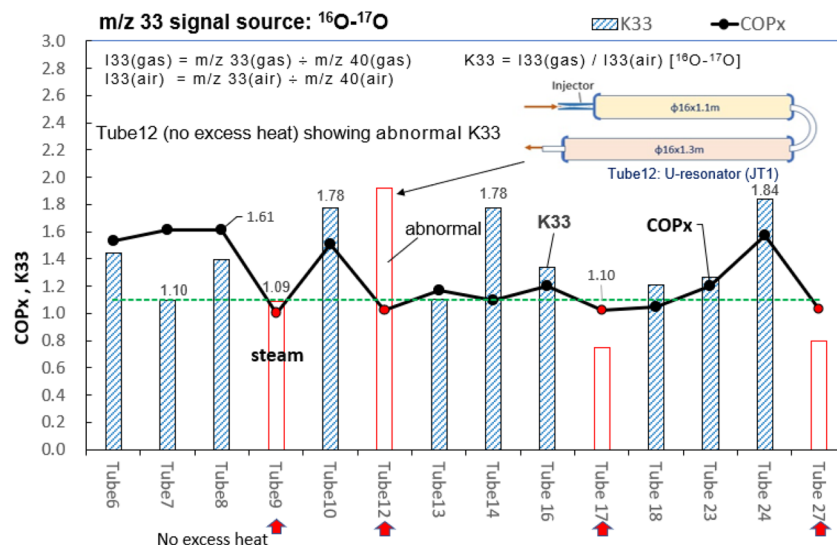


Figure 11. Variation of K33 for gas from different reactors. Using isotope ratio K33 to identify isotope O_2 ($^{16}\text{O}-^{17}\text{O}$).

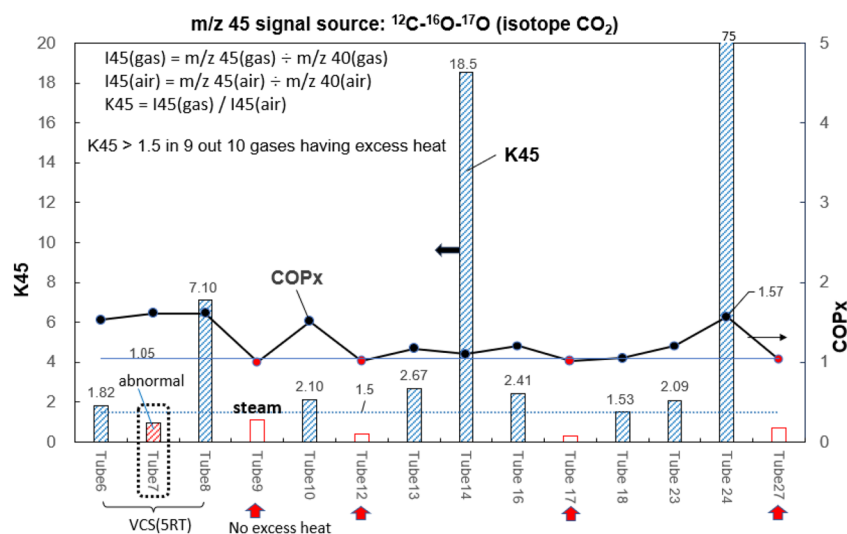


Figure 12. Variation of K45 for gas from different reactors. Using isotope ratio K45 to identify isotope CO_2 ($^{12}\text{C}-^{16}\text{O}-^{17}\text{O}$).

Conclusion

Cavitation may induce implosion of water vapor bubbles using various techniques^{1–10}. In the previous study, we found that the heat exchange process in multiple-pipe heat exchanger produces anomalous excess heat and nuclear transmutation¹¹. Recently, we have tested another 8 reactors and found that they also produce non-condensable gas. We suspected that ^{22}Ne and CO_2 may exist and is from nuclear reactions of water.

Fourteen gas samples were collected from eight reactors to perform mass spectrometry carefully using various methods. Two different methods for the identification of CO_2 were employed, while three different methods are employed for ^{22}Ne . All the results confirm that ^{22}Ne and CO_2 do exist in gas samples from reactors having excess heat.

In answering the question “how ^{22}Ne and CO_2 is produced in water”, we conjecture a possible mechanism and find out that ^{12}C and isotope ^{17}O may be the intermediate. They possibly produce some other isotope compounds in gas from reactors having excess heat. Using isotope ratio analysis, we find out that they are $\text{H}_2\text{O}-17$ (heavy-oxygen water), isotope O_2 ($^{16}\text{O}-^{17}\text{O}$), and isotope CO_2 ($^{12}\text{C}-^{16}\text{O}-^{17}\text{O}$).

We also find that the reactions Eqs. (6)–(8) are the most-probable reactions whose output gas contents coincide with our observations—detected CO_2 and isotopes ^{22}Ne , $\text{H}_2\text{O}-17$, CO_2 ($^{12}\text{C}-^{16}\text{O}-^{17}\text{O}$) and O_2 ($^{16}\text{O}-^{17}\text{O}$), although the detailed mechanism is not known. This needs further basic research. Since the chances of getting

all the present conclusion is so remote, particularly the presence of ^{22}Ne without ^{20}Ne or ^{21}Ne , this work may lead to a new research topic in nuclear science and energy technology if true.

Data availability

All data generated or analyzed during this study are included in this published article and are available from the corresponding author on reasonable request.

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Author contributions

B.J. supervised this research, organized the collaboration, carried out MS data analysis, summarized conclusions and wrote the manuscript. Y.H., P.H. and J.F. designed, built, and tested DHX and resonator-type reactors. M.L. and Y.H. designed, built, and tested VCS reactors. L.T. built the test system. C.K. carried out Neon gas detection. I.F. assisted in test system integration. C.H. helped LENR literature survey. T.R., F.W., and T.F. carried out MS experiment and analysis. K.C. carried out CIMS analysis. Y.T. assisted in reactor analysis. M.Y., L. and S.L. built a test bed and carried out design analysis of resonator reactors. R.W. supervised physical reaction mechanism and assisted the manuscript writing.

Competing interests

The authors declare no competing interests.

Additional information

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